



Forest simulation in industrial CFD codes

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Problem formulation

- Onshore wind power is growing rapidly
- Most suitable locations have already been built upon
- Installation planned in the northern parts of Sweden
 - Lower population density – easier to acquire permit
 - 58% tree coverage [1] & complex terrain
- Expensive and time demanding with physical measurements
 - Complement with CFD simulations
- No industry consensus on how to estimate wind conditions in forested areas
- **Objective is to decrease the uncertainty in the results of the CFD simulations**



Agenda

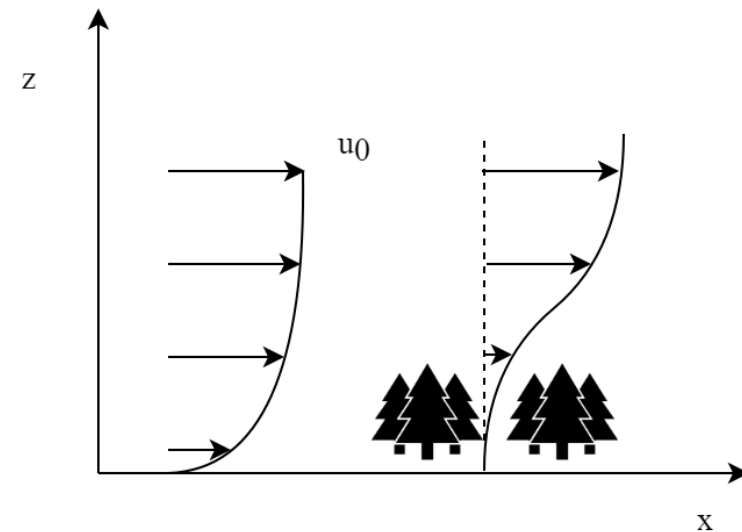
- **Background - Forest simulation and modelling**
- **Sensitivity analysis**
- **Validation with LES data**
- **Simulations for clearings**
- **Case study Rynningsnäs**
- **Conclusions**

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Forest simulation

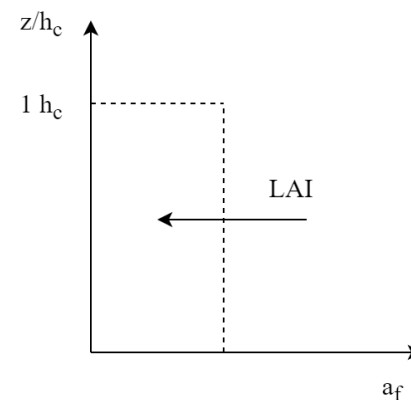
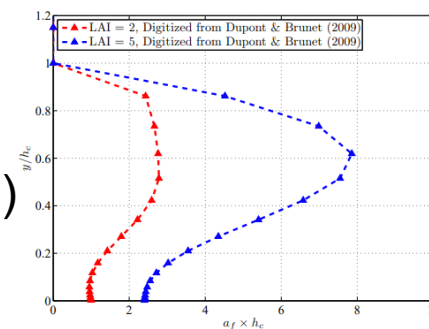
- Inlet profile logarithmic
- Expecting to see momentum being absorbed by the forest
- Higher turbulence regime above forest
- How is forest modelled in CFD tools?



Forest simulation

Accuracy

1. Ideally: No slip BC for all forest with complete cell coverage
 - Computational heavy and not applicable large scale
2. Momentum sink $S_{u,i} = -\rho a_f c_d U^2$
 - a_f , leaf area density [m^2/m^3] $\rightarrow LAI = \int_0^{h_c} a_f dz$
 - Provided from means of aerial scans (skogsstyrelsen)
 - c_d , quantify the drag or resistance of an object
3. Constant a_f over tree height, model used in WindSim
4. No information about the LAI, $C_2 = \text{const.}$



$$C_2 = \frac{LAI}{H} c_d$$

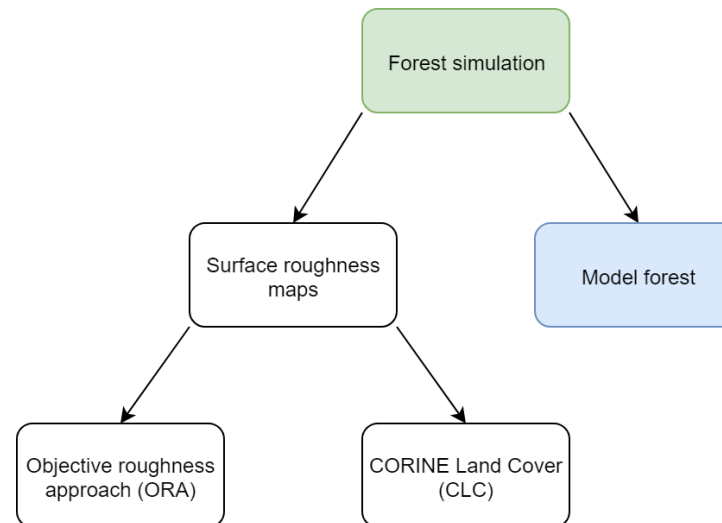
Forest characteristics	LAI	c_d	H [m]	C_2
Very sparse	0,25	0,2	30	0,0017
Slightly sparse	1	0,2	30	0,0067
Slightly dense	4	0,2	30	0,0267
Very dense	16	0,2	30	0,1067

Forest simulation

5. Instead of modelling forest: Imposing roughness maps from data bases

- For instance: CORINE 2006, Wind Atlas etc.
- Objective roughness approach (ORA) - Create roughness maps from tree height

- Modelling the forest is the main focus of the master thesis



Forest modelling

- WindSim, (commercial) software used for this study
- Uses the 3D Reynolds-Average Navier-Stokes (RANS) equation to simulate the flow characteristics

$$1. \quad \frac{\partial U_i}{\partial t} + U_j \frac{\partial U_i}{\partial x_j} = -\frac{1}{\rho} \frac{\partial P}{\partial x_i} + \frac{\partial}{\partial x_j} \left(\nu \frac{\partial U_i}{\partial x_j} - \overline{u'_i u'_j} \right) + \overline{S_{u,i}}$$

$$\overline{S_{u,i}} = -\rho C_2 U |U|$$

- Last term is a momentum sink used to represent impact of e.g. a forest
- C_2 is the forest force resistive constant

Forest modelling

- Solve Reynolds stress by applying Eddy viscosity model
- Introduce k-ε turbulence model + transport equation k and ε
- Introduce turbulence sources

$$2. \quad \tau_{ij} = -\overline{\rho u'_i u'_j} = \mu_t \left(\frac{\partial U_i}{\partial x_j} + \frac{\partial U_j}{\partial x_i} \right) - \frac{2}{3} \rho k \delta_{ij}$$

$$3. \quad \mu_t = \rho C_\mu \frac{k^2}{\varepsilon}$$

4. Rate of change = production - destruction + transportation + turbulent sources

$$4. \quad \left\{ \begin{array}{l} \frac{Dk}{Dt} = P - \varepsilon + \frac{\partial}{\partial x_j} \left(\left(\nu + \frac{\nu_t}{\sigma_k} \right) \frac{\partial k}{\partial x_j} \right) + S_k \\ \frac{D\varepsilon}{Dt} = (C_{\varepsilon 1} P - C_{\varepsilon 2} \varepsilon) \frac{\varepsilon}{k} + \frac{\partial}{\partial x_j} \left(\left(\nu + \frac{\nu_t}{\sigma_\varepsilon} \right) \frac{\partial \varepsilon}{\partial x_j} \right) + S_\varepsilon \end{array} \right.$$

$$5. \quad \left\{ \begin{array}{l} S_k = C_2 (\beta_P |U|^3 - \beta_D |U|k) \\ S_\varepsilon = C_2 (C_{\varepsilon 4} \beta_P \frac{\varepsilon}{k} |U|^3 - C_{\varepsilon 5} \beta_D |U|\varepsilon) \end{array} \right.$$

Empirically derived parameters

- $C_\mu = 0,09$
- $C_{\varepsilon 1} = 1,44$
- $C_{\varepsilon 2} = 1,92$
- $\sigma_k = 1,0$
- $\sigma_\varepsilon = 1,0$

Empirically derived parameters from Sanz 2003 [2]

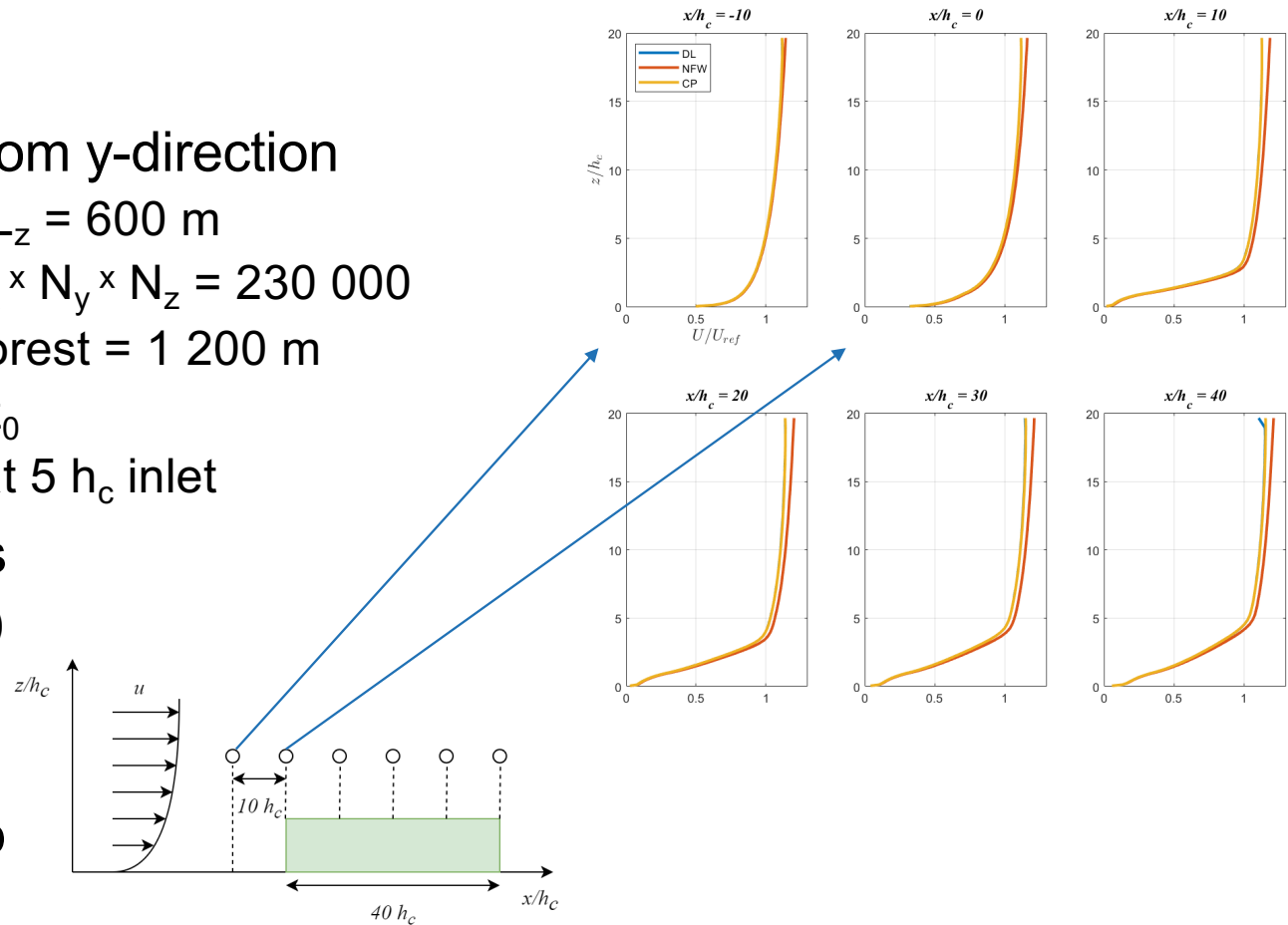
- $\beta_P = 1,0$
- $\beta_D = 6,51$
- $C_{\varepsilon 4} = 1,24$
- $C_{\varepsilon 5} = 1,24$

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Top boundary condition

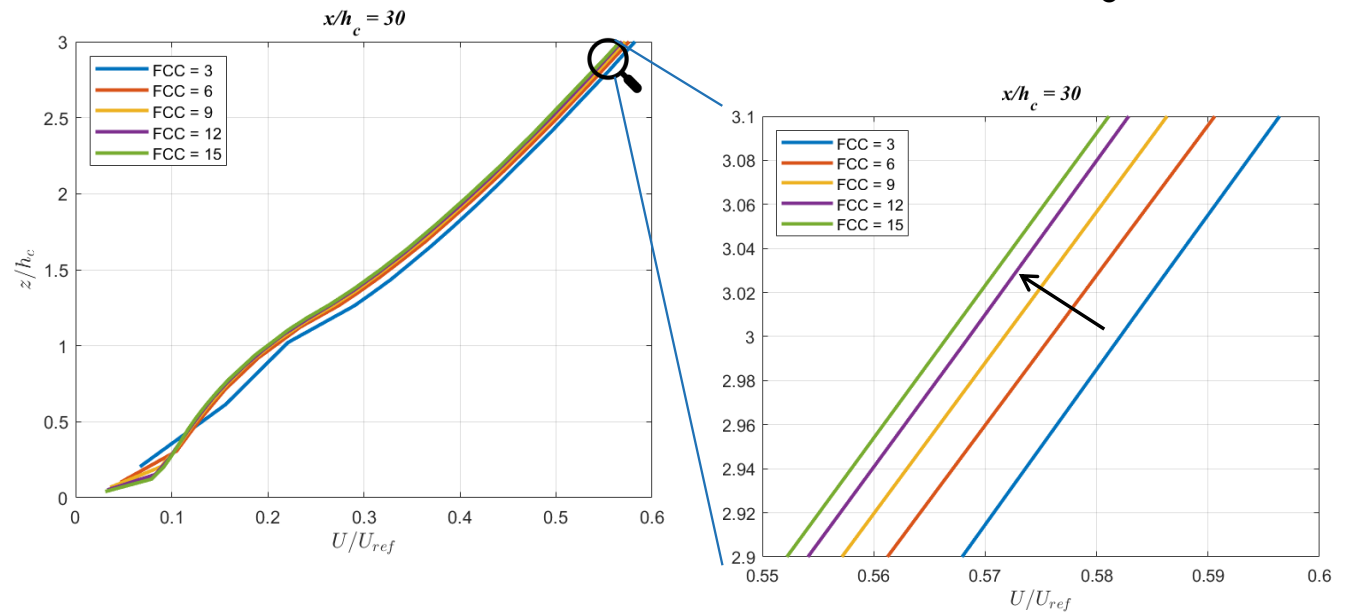
- 3D domain, no impact from y-direction
 - $L_x = 2\,400$ m, $L_y = 40$ m, $L_z = 600$ m
 - Cell size x-y = 5×5 m, $N_x \times N_y \times N_z = 230\,000$
 - $h_c = 30$ m, length of the forest = $1\,200$ m
 - Full forest with constant z_0
 - Wind speed normalized at $5 h_c$ inlet
- Top boundary conditions
 - Constant pressure ($p = c$)
 - ~~No friction wall ($\tau = 0$)~~
 - ~~Diffusive link (p & $\tau = c$)~~
- Avoid physical speed-up



Forest cell count

- Same domain as for top boundary condition
- Varying amount of cells in vertical direction of forest, between 3 – 15
- Limited amount of cells to employ in WindSim (60) – trade off
- Middle of the forest: FCC = 3 is 1,8% higher than FCC = 12 at $3 h_c$

- Fewer amount of cells overestimates the wind speed

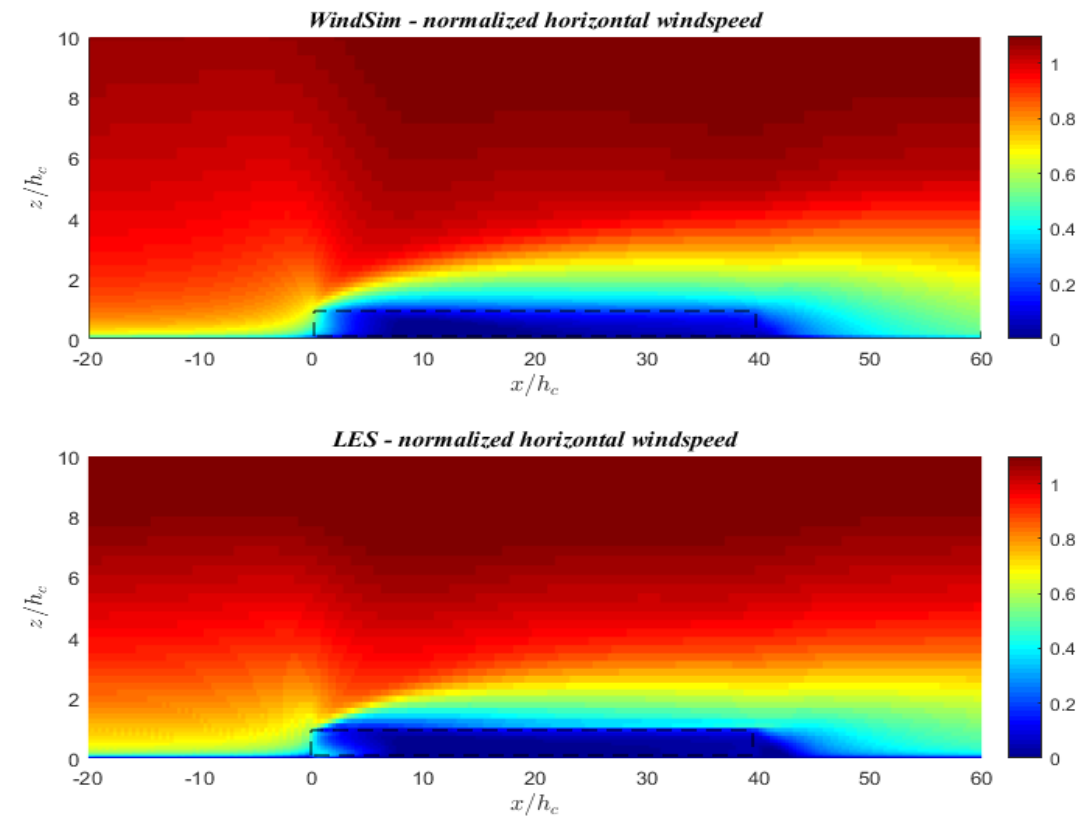


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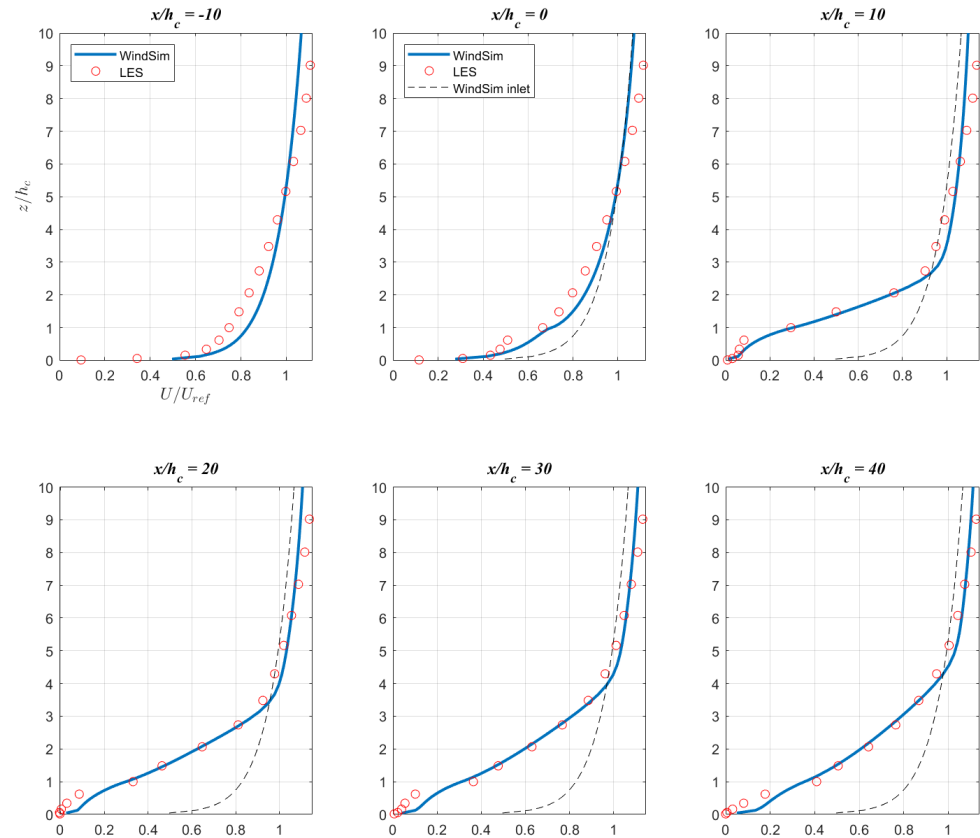
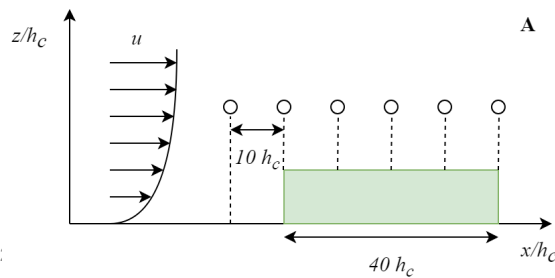
Validation with LES data

- LES data provided from Antonio [3]
- Same domain as in sensitivity analysis
- Full forest, LAI = 2 (slightly sparse)
 - Reduction of wind speed in front of the forest
 - Speed reduction in forest region
 - Similar shape profile after leading edge of the forest
 - Similar recovery after forest



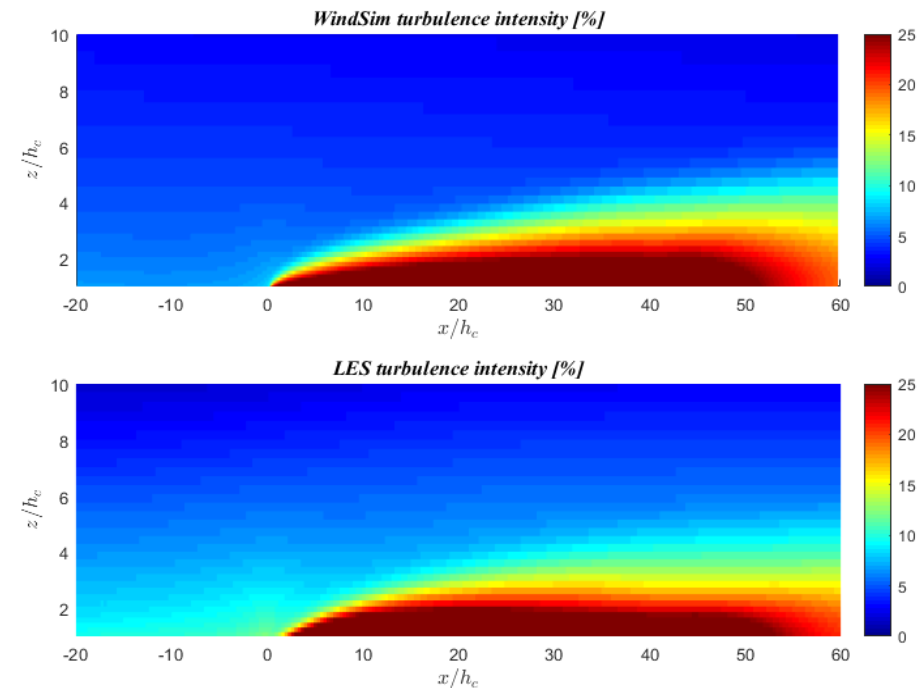
Validation with LES data

- Extracting vertical wind profiles
- Inlet is different due to laminar/turbulent flow
 - WindSim continuously develops the wind profile
- Different LAD profile – reduction of wind speed inside forest
- Very good agreement above canopy



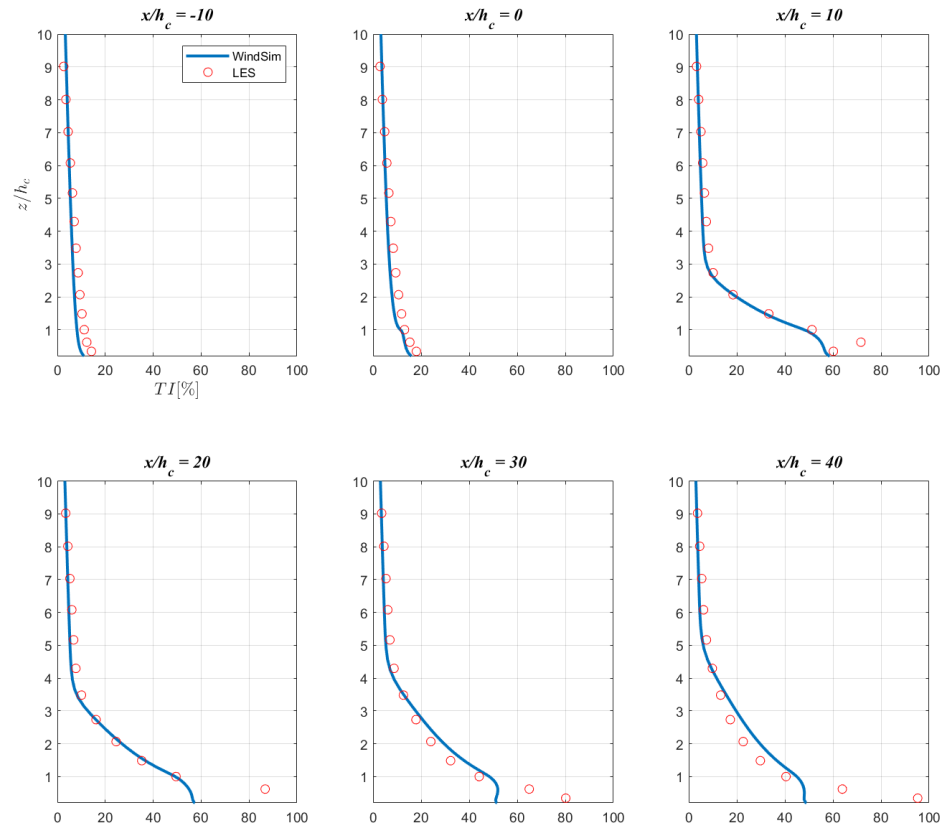
Validation with LES data

- $TI = \frac{\sqrt{k}}{U} \cdot 100$, dimensionless
- Figure starts at $z/h_c = 1$
- High turbulence region to $3 h_c$
- Forest affects up to $5 h_c$
- Good agreement
 - Except at the leading edge of the canopy
 - Accurately identify regions with low TI



Validation with LES data

- Good agreement above forest and at inlet
 - Similar gradient at all x/h_c
- Inside of the forest LES displays a higher TI

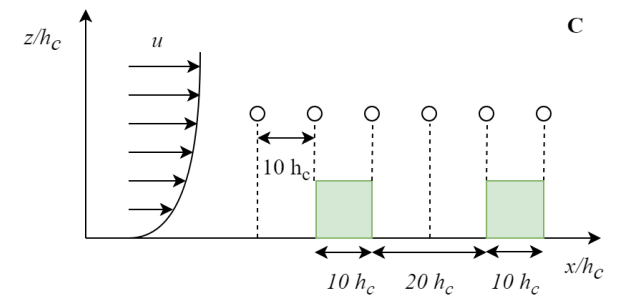
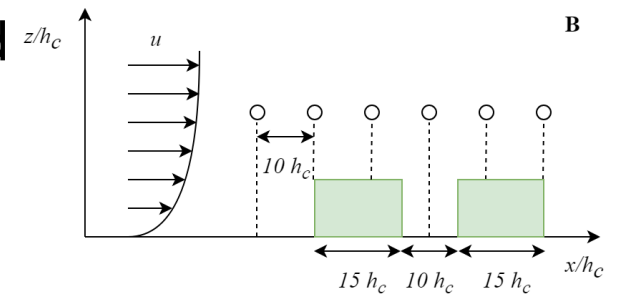
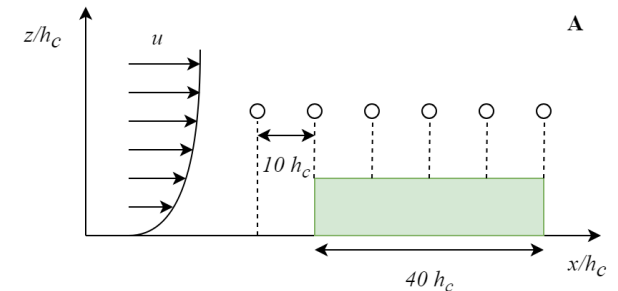


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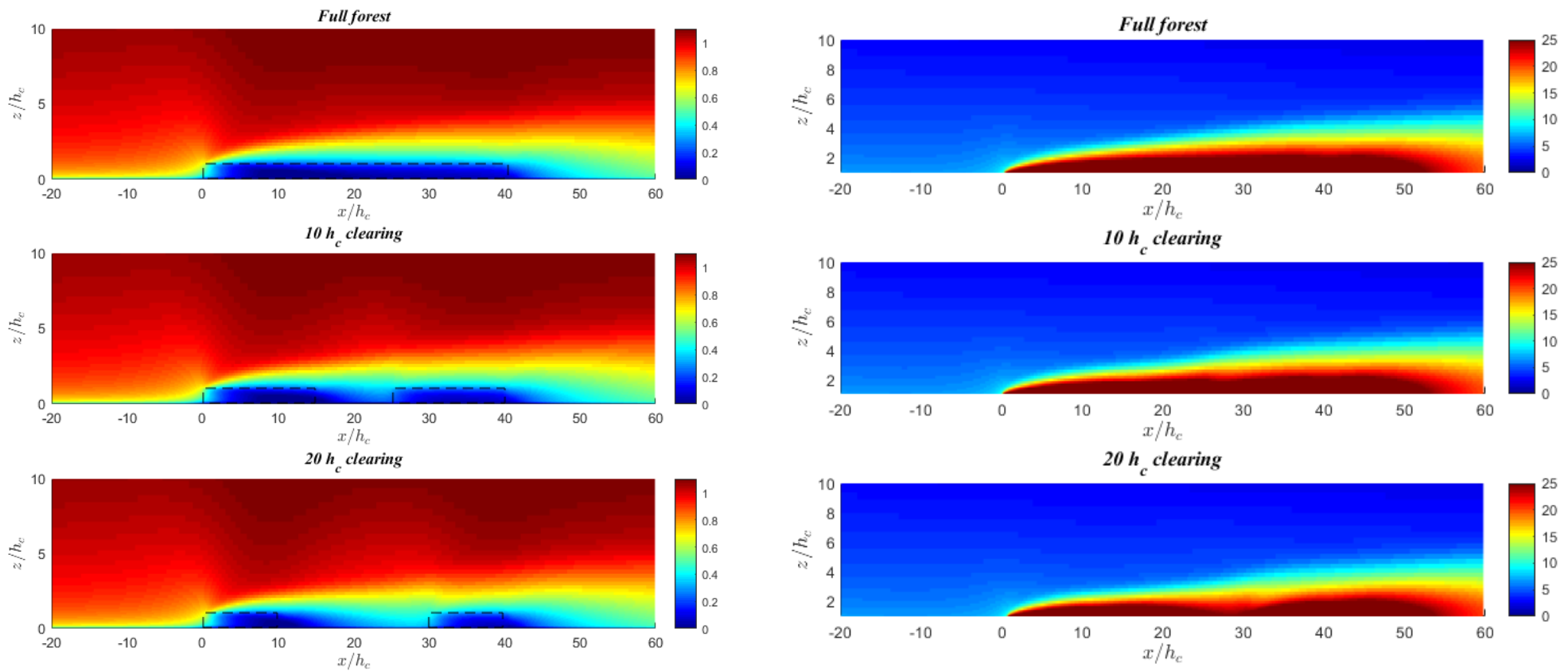
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WindSim clearing results

- Forest is not always present but usually followed by clearings, which is why it is important to understand their influence on the wind profile and TI
- Varying clearing sizes between **full forest**, $10 h_c$ and $20 h_c$
- With both LAI = 2 (slightly sparse) and LAI = 5 (slightly dense) forest

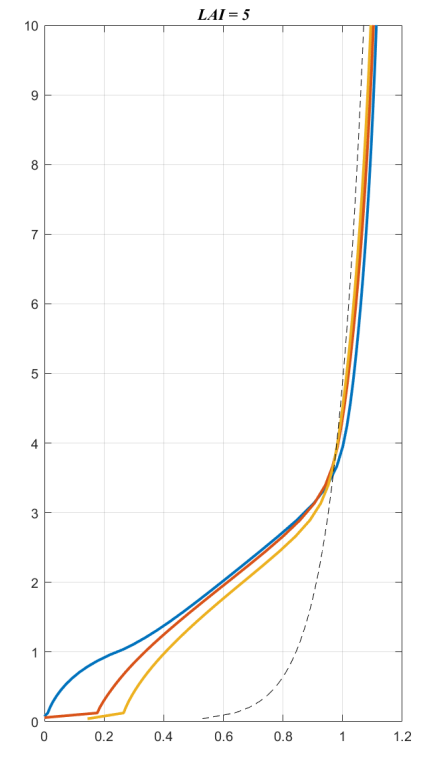
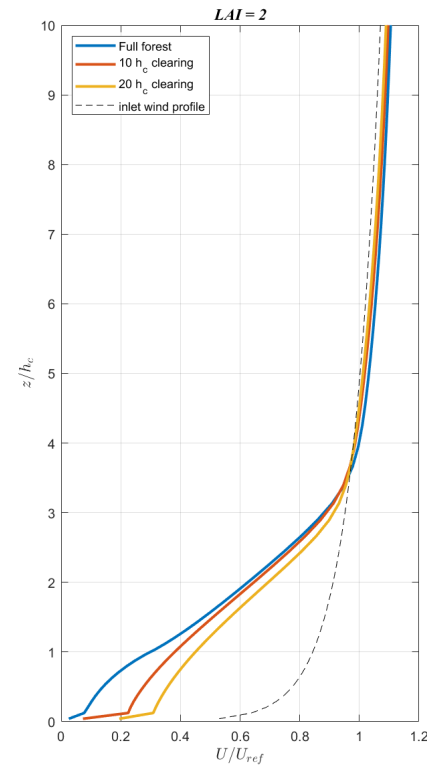


WindSim clearing results



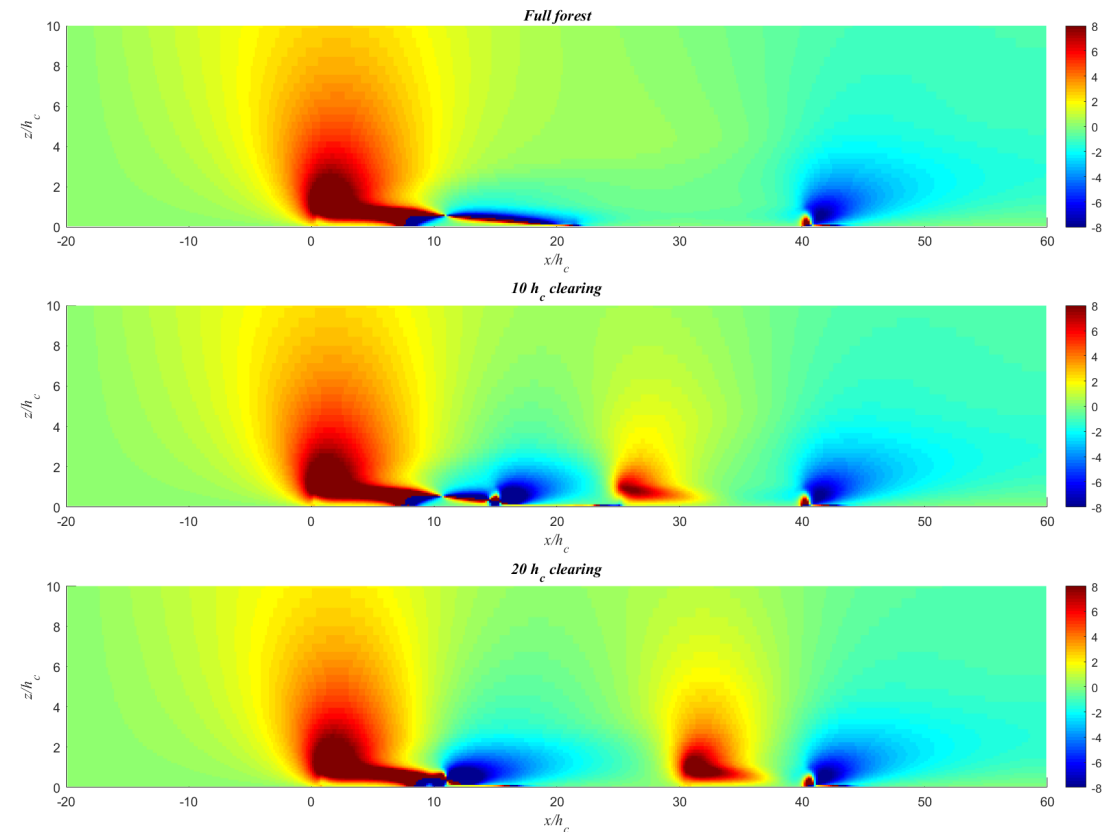
WindSim clearing results

- Profiles in the middle of the clearing
- Similar results for LAI = 2 and 5
 - Slightly higher horizontal wind speed for higher LAI above $4 h_c$
 - Full forest yields the highest horizontal wind speed above $4 h_c$
 - Higher wind speed below $3,5 h_c$ the larger the clearing



WindSim clearing results

- Displaying wind direction $\pm 8^\circ$ with regards horizontal plane
 - IEC recommends angle $< |8|$ [5]
 - 8° at approximately $3 h_c$ for LAI = 5, lower for LAI = 2
- Similar angle at the leading and trailing edge of the canopy for all clearings
- Larger clearing yields higher wind angle inside the clearing

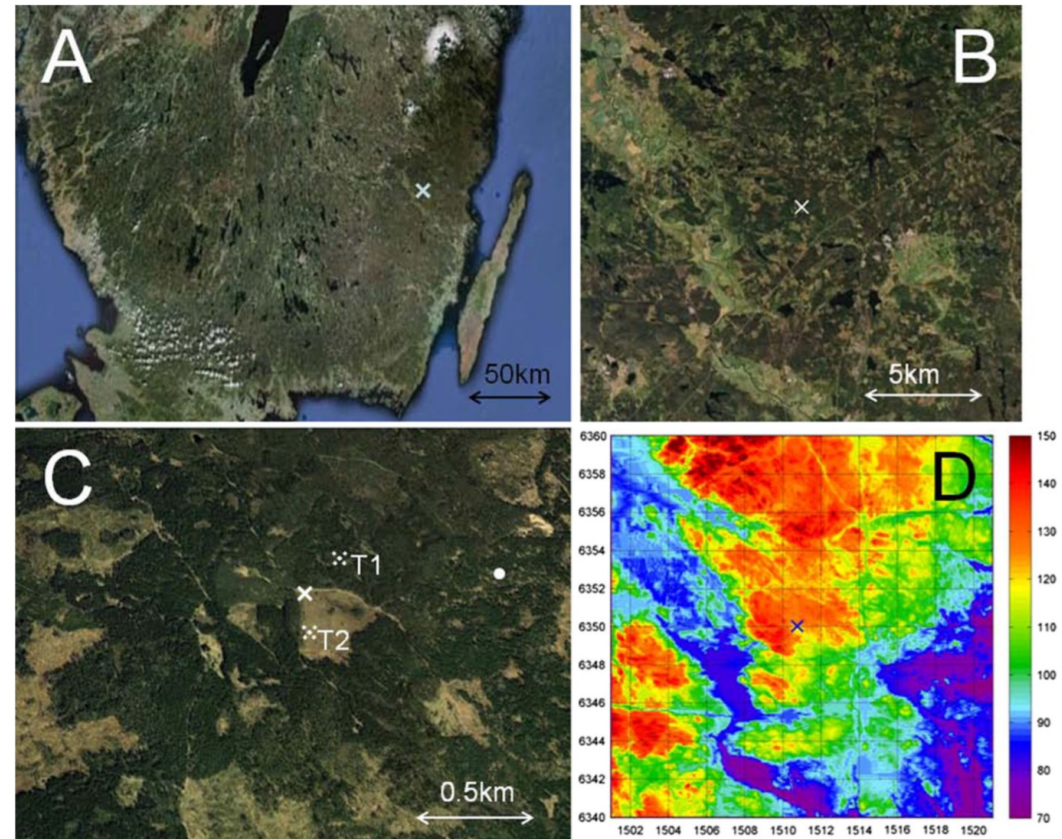


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Case study

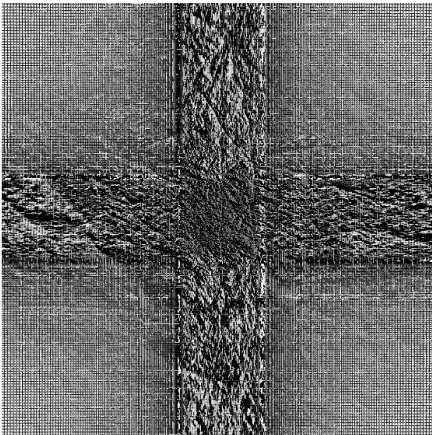
- Swedish forest Rynningsnäs
- Atmospheric measurements:
 - PAI, tree height and elevation
- Consist mainly of Scot Pines
- Simulating five different cases
 1. Bin discretization (RDV60)
 2. Industrial standard (RDV6)
 3. Constant C_2
 4. ORA20d
 5. Corine



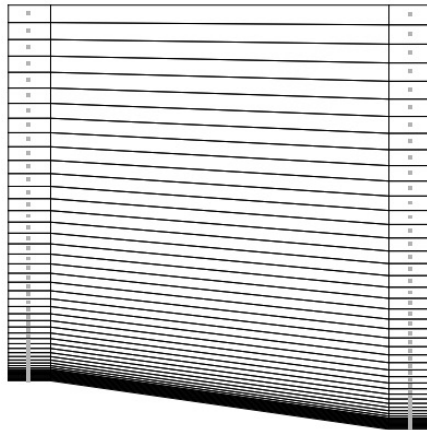
Case study – 3D Domain setup

- Domain size 30 × 30 km, recommendation to use 15 km upstream direction
- Refinement 2 × 2 km around mast, data from 100, 240 and 290°
- Refinement in the vertical direction, equispaced in forest
- Roughly 11 M cells

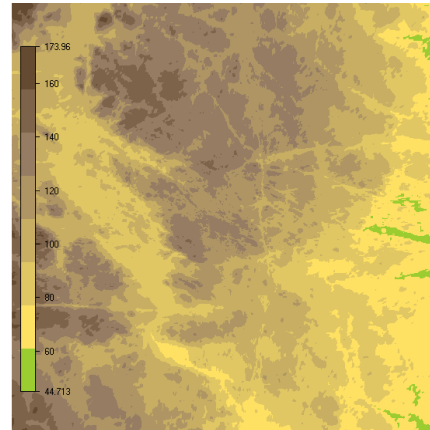
Grid (xy)



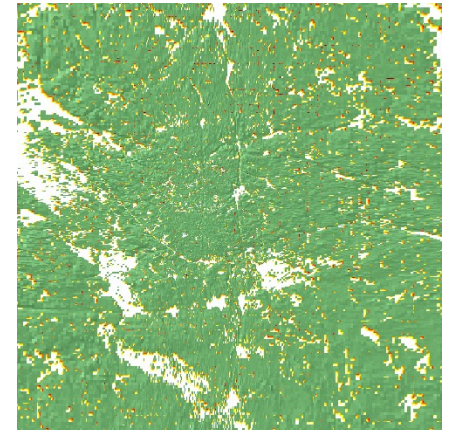
Grid (z)



Elevation height



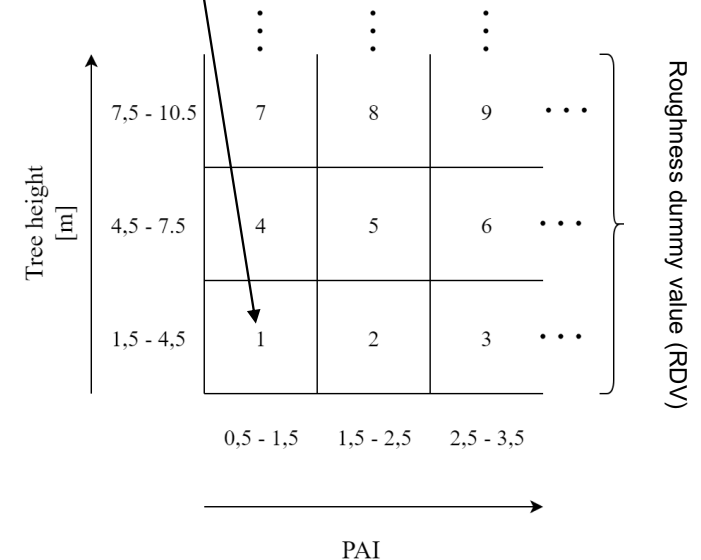
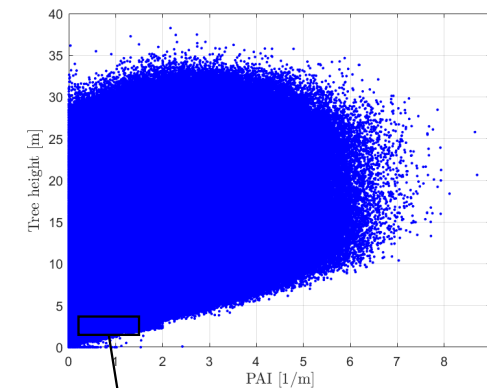
Forest



Case study – Bin discretization

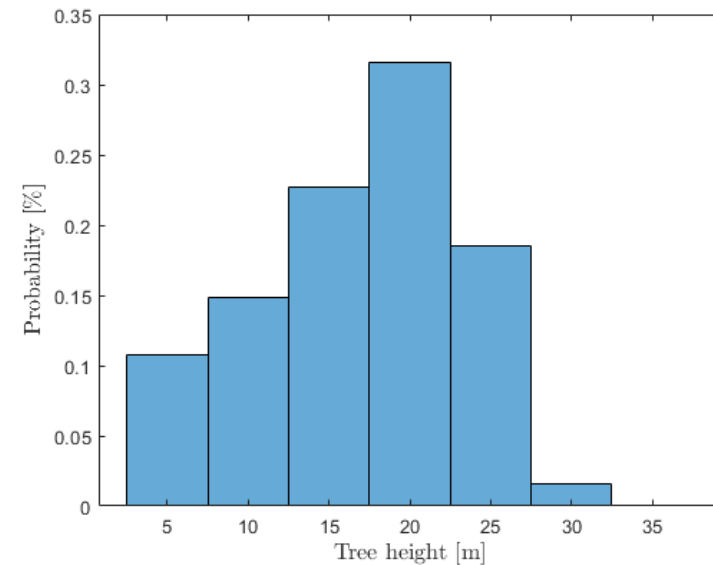
RDV60

- Problem: C_2 matrix can't be implemented directly in WindSim. Simplifications are required
- Poor correlation between tree height and PAI (used in same manner as LAI)
- Instead of 1 PAI per tree height bin
→ several PAI per tree height bin
- 10 tree height bins, each bin has 6 PAI amounting to 60 RDVs (roughness dummy values)
- Forest cell count 12



Case study – Industrial method RDV6

- Easier with $PAI \propto h_c$
- Resulting in six tree height bins with six unique C_2 values
 - Forest height below 2,5 m and PAI below 0,1 was neglected and considered as roughness length = 0,05

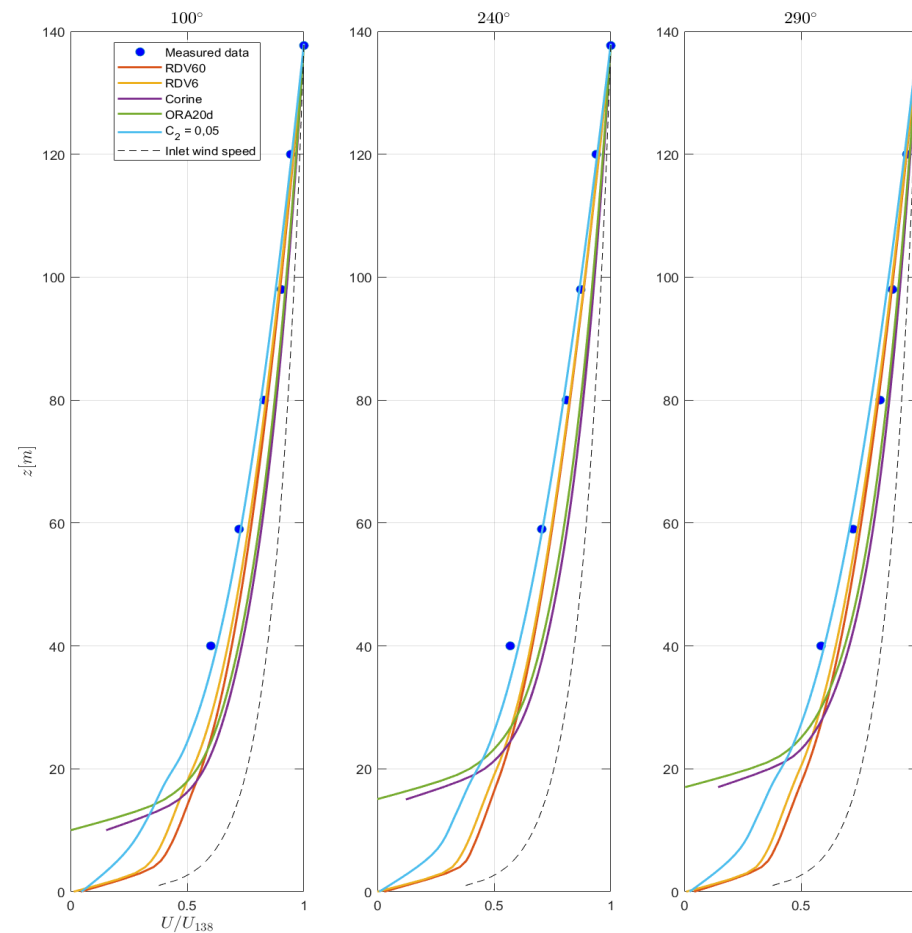


Case study – Auxiliary simulations

1. $C_2 = 0,05$: Some industries apply a constant C_2 for the whole forest
2. ORA20d: Objective roughness approach (ORA), roughness map from dividing tree height with a factor of 10 and adding the displacement height [6]
 - Resolution 20×20 m in the refinement
3. Imposing only roughness map from Corine 2006 database,
 - Resolution of the roughness map was 100×100 m

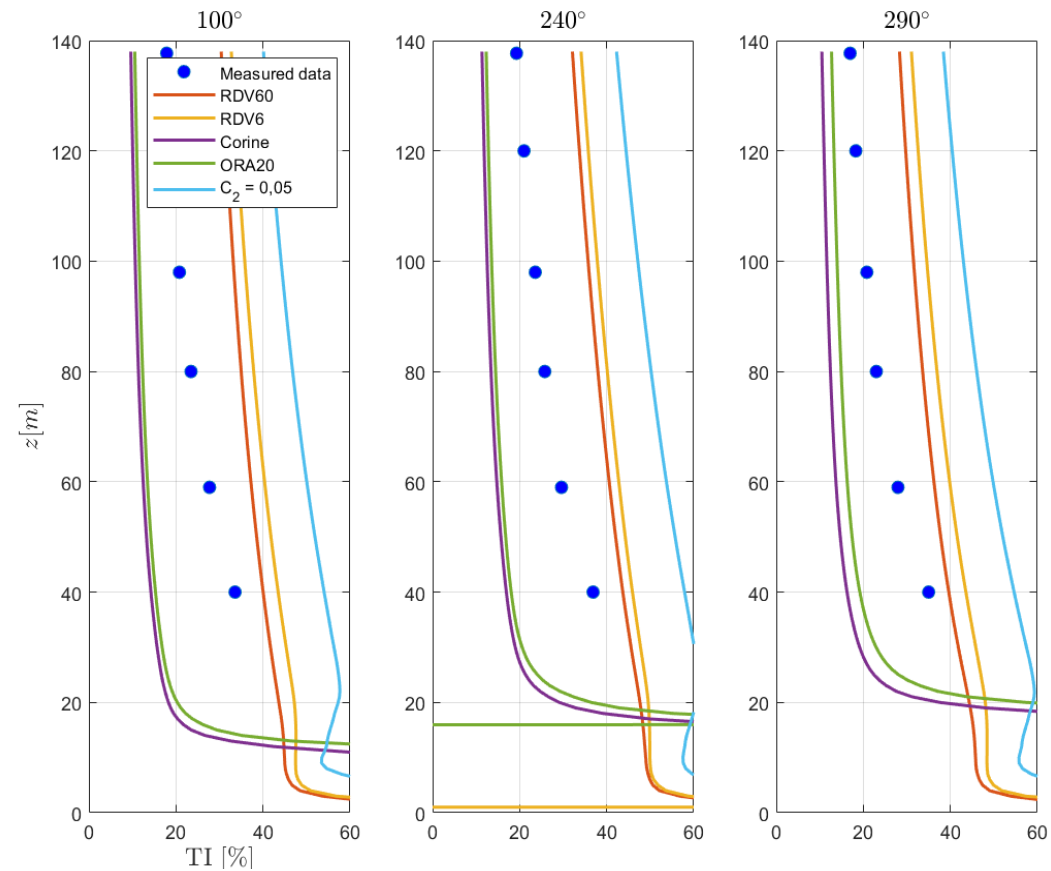
Case study – horizontal wind speed

- Data normalized with U_{138} of measured data
- Similar share for RDV60 and RDV6
 - Good agreement above 80 m
 - Overestimates below 80 m
- Best agreement reached with $C_2 = 0,05$
- ORA20d and Corine overestimates wind speed



Case study - TI

- Poor agreement with measured data for RDV6 and RDV60
- Constant C_2 severely overestimates the TI
- Roughness map approach underestimates the TI
 - ORA20d slightly better estimation than Corine



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Conclusions for the case study

- RDV60 had better agreement with TI than RDV6
 - RDV6 slightly better estimation of the horizontal wind speed
- Best estimation for wind speed was achieved with constant $C_2 = 0,05$
 - Indicates that the impact of the forest is underestimated, most likely due to a too low drag coefficient (0,2)
- Roughness map approach
 - ORA20d yielded better horizontal wind speed and TI than Corine
- Overall: modelling the forest resulted in better agreement with the measured data
- Overestimated TI yields an underestimated horizontal wind speed and vice versa

References

- [1]: Fridman, J. (2018). "Forest statistics 2018". In: Official Statistics of Sweden, Swedish University of Agricultural Sciences, ISSN 0280-0543, p. 81.
- [2]: Sanz, C. (2003). A note on $k - \epsilon$ modelling of vegetation canopy air-flows, page 191-197. Tech. rep. No.108. Kluwer Academic Publishers.
- [3]: Segalini, A., T. Nakamura, and K. Fukagata (2016). "A Linearized $k - \epsilon$ Model of Forest Canopies and Clearings". In: Boundary-Layer Meteorology 161.3. issn: 1573-1472. doi:10.1007/s10546-016-0190-5. url: <https://doi.org/10.1007/s10546-016-0190-5>.
- [4]: Enevoldsen, P., C. Meissner, and V. Jothiprakasham (2017). Validation of CFD forest simulations based on a global forest parameter database. Power point presentation. WindEurope: Flow modelling for complex conditions
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- [6]: Floors, R., P. Enevoldsen, N. Davis, J. Arnvist, and E. Dellwik (2018). "From lidar scans to roughness maps for wind resource modelling in forested areas". In: Wind Energy Science 3.1, pp. 353–370. doi:10.5194/wes-3-353-2018. url: <https://www.wind-energ-sci.net/3/353/2018/>.